

HYPERBOLIC FREE-EVOLUTION SCHEMES

GENERALIZED HARMONIC GAUGE (HMG) AND SYMM. HYP. SCHEME

Consider the Ricci tensor expression in some coordinate system

$$R_{ab} = -\frac{1}{2} g^{cd} \partial_c \partial_d g_{ab} + \nabla_{(a} \Gamma_{b)} + g^{cd} g^{ef} (\partial_e g_{ca} \partial_f g_{db} - \Gamma_{ace} \Gamma_{bdf})$$

where $\Gamma_a = g^{bc} \Gamma_{abc}$ and Γ_{abc} are the Christoffel symbols, and

$$\nabla_a \Gamma_b = \partial_a \Gamma_b - g^{cd} \Gamma_{ceb} \Gamma_d$$

The terms (x) are those containing the 2nd derivatives of the metric:

$$g^{cd} \partial_c \partial_d g_{ab} \approx \square g_{ab}$$

$\nabla_{(a} \Gamma_{b)}$ can break hyperbolicity of Einstein equations in vacuum:

$$\boxed{0 = R_{ab} \approx -\frac{1}{2} \square g_{ab} + \dots}$$

Consider now harmonic coordinates x^α [de Donder 1921]:

$$\square x^\alpha = 0$$

which means

$$0 = g^{ab} \nabla_a \nabla_b x^\alpha \stackrel{\uparrow}{=} g^{ab} \nabla_a (\partial_b x^\alpha) = g^{ab} \left[\underbrace{\partial_a (\partial_b x^\alpha)}_{\delta_b^\alpha} - \underbrace{\partial_e x^\alpha \Gamma_{ab}^e}_{\delta_e^\alpha} \right] =$$

x^α is not a vector

$$= 0 - g^{ab} \Gamma_{ab}^\alpha = -\Gamma^\alpha$$

$$\Gamma^\alpha = 0 \Rightarrow$$

$$\boxed{g^{cd} \partial_c \partial_d g_{ab} = 2 g^{cd} g^{ef} (\partial_e g_{ca} \partial_f g_{db} - \Gamma_{ace} \Gamma_{bdf})}$$

GR is a manifestly hyperbolic system in HMG.

More in general one can use a generalized harmonic gauge (GHG) in the form:

$$-\Gamma^a = H^a$$

where $H^a(x^\mu)$ can be

- a prescribed function
- a field that satisfies symm. hyp. equations

and obtain:

$$R_{ab} = -\frac{1}{2} \square g_{ab} + \nabla_{(a} H_{b)} + \text{low order derivative terms}$$

which is also symm. hyperbolic $\rightarrow$ GHG system.

Define the quantity

$$Z_a := H_a + \Gamma_a$$

if we consider Z_a as algebraic constraint the GHG system can be written:

$$\begin{cases} 0 = R_{ab} - \nabla_{(a} Z_{b)} \\ 0 = Z_a \end{cases}$$

How does the constraint evolve?

$$\begin{aligned} 0 &= \text{Tr} [R_{ab} - \nabla_{(a} Z_{b)}] = g^{ab} R_{ab} - g^{ab} \nabla_{(a} Z_{b)} = R - \frac{1}{2} g^{ab} (\nabla_a Z_b + \nabla_b Z_a) = \\ &= R - \frac{1}{2} Z^a \nabla_a \text{Tr} g \end{aligned}$$

$$\begin{aligned} 0 &= R_{ab} - \nabla_{(a} Z_{b)} - \text{Tr} [\dots] \frac{1}{2} g_{ab} \\ &= R_{ab} - \frac{1}{2} R g_{ab} - \nabla_{(a} Z_{b)} + \frac{1}{2} \nabla^d Z_d g_{ab} \end{aligned}$$

$$0 = \nabla^a \left\{ R_{ab} - \nabla_{(a} Z_{b)} - \text{Tr} [\dots] \frac{1}{2} g_{ab} \right\} =$$

$$0 = \underbrace{\nabla^a R_{ab} - \frac{1}{2} g_{ab} \nabla^a R - \frac{1}{2} \nabla^a \nabla_a Z_b - \frac{1}{2} \nabla^a \nabla_b Z_a + \frac{1}{2} g_{ab} \nabla^a \nabla^a Z_d}_{=0, \text{ Bianchi identity}} =$$

$$= -\frac{1}{2} \nabla^a \nabla_a Z_b + \frac{1}{2} g_{ab} \nabla^a \nabla^d Z_d - \frac{1}{2} \nabla^a \nabla_b Z_a =$$

$$= g^{ac} \nabla_c \nabla_b Z_a \stackrel{\substack{\uparrow \\ \text{Ricci identity}}}{=} g^{ac} (\nabla_b \nabla_c Z_a) - g^{ac} R^f_{acb} Z_f = \nabla_b \nabla^a Z_a - R^f_b Z_f$$

$$= -\frac{1}{2} \nabla^a \nabla_a Z_b + \frac{1}{2} \cancel{\nabla_b \nabla^a Z_a} - \frac{1}{2} \cancel{\nabla_b \nabla^a Z_a} + \frac{1}{2} R_{bf} Z^f =$$

$$= +\frac{1}{2} \nabla^a \nabla_a Z_b + \frac{1}{2} R_{bf} Z^f = 0$$

This equation guarantees that for $Z_a = 0 = \dot{Z}_a$ the constraint $Z_a = 0$ remains during the evolution.

We have already found this equation: the Z_4 system!

Indeed GR is locally equivalent to the Z_4 system, the difference is that:

- Z_4 : there is no gauge fix, the field Z_a is evolved;

- GR: $Z_a = 0$ is an algebraic constraint.

If one takes Z_4 and fix $Z_a = H_a + \Gamma_a$, then one obtains a GR solution in harmonic gauge.

The Hamiltonian and momentum constraints in GR can be formulated using a 4-momentum constraint:

$$C_a := \left(R_{ab} - \frac{1}{2} g_{ab} R \right) n^b = 0$$

First order formulation [Alvi 2002] [Lindblom 2006]:

$$\pi_{ab} := -n^c \partial_c g_{ab}$$

$$\Phi_{iab} := \partial_i g_{ab}$$

Principal part:

$$\begin{cases} \partial_t g_{ab} - \beta^k \partial_k g_{ab} \cong 0 \\ \partial_t \pi_{ab} - \beta^k \partial_k \pi_{ab} \cong 0 \\ \partial_t \Phi_{iab} - \beta^k \partial_k \Phi_{iab} + \alpha \partial_i \pi_{ab} \cong 0 \end{cases}$$

define: $u = (g_{ab}, \Phi_{iab}, \pi_{ab}) \rightarrow \partial_t u + \lambda^k \partial_k u = s$

Notes:

- In numerical applications the constraint $C_{iab} := \partial_i g_{ab} - \Phi_{iab}$ is observed to grow. Numerical evolutions are different from mathematical statement (necessary but not sufficient) as additional complications can arise from discretization errors.
- this formulation can be augmented with constraints damping terms, as we have discussed with the $\Sigma 4$ scheme.
- Pretorius 2006 breakthrough used ADM with constraint damping in 2nd-order form.
- The above formulation can produce shocks since it is not linearly degenerate ($\nabla \lambda_i \cdot r_i = 0$). For example the (ti)-constraint is

$$\partial_t \beta^i - \beta^k \partial_k \beta^i \cong 0$$
 i.e. Burgers-type of equation.
- A formulation that is i) 1st-order symm-hyperbolic ii) linearly degenerate and with C_{iab} numerically stable in different tests has been proposed by Lindblom 2006.

FROM GHG AND "ADM" TO BSSN

- GHG system is hyperbolic but with gauge fixed.
- 3+1 GR "ADM" is nearly hyperbolic but with gauge freedom (α, β^i) .

How can we build something strongly/symmetrically hyperbolic given a generic gauge?
(note we assume the gauge is in strongly/symmetrically hyperbolic form, or can be put)

Let us consider the 3+1 decomposition and follow some of the ideas of GHG.

$$(\partial_t - \beta^j \partial_j)^2 \gamma_{ij} \approx R_{ij} + \dots$$

$$\approx \underbrace{-\frac{1}{2} \Delta \gamma_{ij}}_{\text{this is a "good" term}} + \underbrace{\gamma_{ik} \partial_j \partial_t \gamma^{kl} + \gamma_{jk} \partial_i \partial_t \gamma^{kl}}_{\text{these are problematic terms, exactly as for the derivation of GHG from 4D equations ...}} + \dots$$

[Nokamura, Oohara, Kojima 1987] $\rightarrow$ introduce auxiliary variables

$$F^k \approx \partial_t \gamma^{kl}$$

such that the system is strongly hyperbolic
without specifying the gauge

The problem reduces to finishing an equation for F^k ...

... a solution is to combine the evolution equation for γ_{ij} ~~in the ADM formalism~~

$$\partial_t F^k \sim \partial_t \partial_i \gamma^{ki} \sim \partial_i \partial_t \gamma^{ki} \sim \partial_i K^{ki}$$

and e.g. use the constraint (momentum)

... analogously one can remember the Z4 system and $F^k \sim Z^k$ so that

$$\partial_t F^k \sim \partial_t Z^k \propto (\text{mom. constraint}) -$$

Let us now play the same game with the 3+1 conformal decomposition of ADM eqs.:

$$\Delta^k_{ij} := \underbrace{\tilde{\Gamma}^k_{ij}}_{\substack{\text{of the flat metric} \\ \text{REM: } \Delta^i_{jk} \text{ depend on the background metric}}} - \tilde{\Gamma}^k_{ij} = \frac{1}{2} \tilde{\gamma}^{kl} (\partial_i \tilde{\gamma}_{kl} + \partial_j \tilde{\gamma}_{kl} - \partial_l \tilde{\gamma}_{ij})$$

REM: Δ^i_{jk} depend on the background metric.

$$\tilde{R}_{ij} = \partial_k \Delta^k_{ij} - \Delta^k_{ik} \Delta^l_{lj} \approx -\frac{1}{2} \tilde{\gamma}^{kl} (\partial_k \partial_l \tilde{\gamma}_{ij} + \tilde{\gamma}_{ik} \partial_j \partial_l \tilde{\gamma}^{kl} + \tilde{\gamma}_{jk} \partial_i \partial_l \tilde{\gamma}^{kl}) + \dots$$

and again

$$(\partial_t - \partial_\beta)^2 \tilde{\gamma}_{ij} \approx \tilde{R}_{ij} + \dots$$

[Shibata & Nakamura 1995]

[Bonnor & Shapiro 1996]

$$\longrightarrow \boxed{-\tilde{\Gamma}^l := \partial_l \tilde{\gamma}^{kl}}$$

Auxiliary conformal variables

To obtain an equation one can either use $\mathbb{Z}_4$ (zhc) or follow the ideas sketched above:

$$\partial_t \tilde{\gamma}^{ij} = 2\alpha \tilde{A}^{ij} + \beta^k \partial_k \tilde{\gamma}^{ij} - \tilde{\gamma}^{kj} \partial_k \beta^i - \tilde{\gamma}^{ik} \partial_k \beta^j + \frac{2}{3} \partial_k \beta^k \tilde{\gamma}^{ij}$$

take the divergence:

$$\partial_i (\partial_t \tilde{\gamma}^{ij}) = \partial_t \partial_i \tilde{\gamma}^{ij} = \partial_t (-\tilde{\Gamma}^j_i) = 2\alpha \underbrace{\partial_i \tilde{A}^{ij}}_{(c)} + \dots$$

use the mom. constraint:

$$(c) \partial_j \tilde{A}^{ij} = -6 \tilde{A}^{ij} \partial_j \ln \psi + \frac{2}{3} \tilde{D}^i_k + 2\pi \psi^4 p^i = \partial_j \tilde{A}^{ij} + \Delta^i_{jk} \tilde{A}^{kj}$$

The full BSSN (or BSSNOK) system is

$$\left\{ \begin{array}{l} \mathcal{L}_m \psi = \frac{\psi}{6} \tilde{D}_i \beta^i - \alpha K \\ \mathcal{L}_m \tilde{\gamma}_{ij} = -2\alpha \tilde{A}_{ij} - \frac{2}{3} \tilde{D}_k \beta^k \tilde{\gamma}_{ij} \\ \mathcal{L}_m K = \dots \\ \mathcal{L}_m \tilde{A}_{ij} = \dots \\ \mathcal{L}_m \tilde{\Gamma}^i = \frac{2}{3} \tilde{D}_k \beta^k \tilde{\Gamma}^i + \tilde{\gamma}^{jk} \tilde{D}_j \tilde{D}_k \beta^i + \frac{1}{3} \tilde{\gamma}^{ij} \tilde{D}_j \tilde{D}_k \beta^k - 2 \tilde{A}^{ij} \tilde{D}_j \alpha + \\ - 2\alpha [8\pi \psi^k P^i - \tilde{A}^{jk} \tilde{D}_{jk}^i - 6 \tilde{A}^{ij} \tilde{D}_j \ln \psi + \frac{2}{3} \tilde{\gamma}^{ij} \tilde{D}_j K] \end{array} \right.$$

+ gauge (to be specified)

+ Hamiltonian and momentum constraints $C_0 = 0 = C_i$

+ Algebraic constraints

$$\left\{ \begin{array}{l} \det \tilde{\gamma}_{ij} = f \\ \tilde{\gamma}^{ij} \tilde{A}_{ij} = 0 \\ \tilde{\Gamma}^i + \tilde{D}_j \tilde{\gamma}^{ij} = 0 \end{array} \right.$$

Note: This is analogous to Z4 but with an equation less $[\dot{\Phi} = c_0]$ and with $\tilde{\Gamma}^i$ playing the role of Z_i .

1. The first part of the paper is devoted to a general discussion of the problem.

2. The second part is devoted to a detailed analysis of the results.

3. The third part is devoted to a discussion of the conclusions.

4. The fourth part is devoted to a discussion of the future work.

5. The fifth part is devoted to a discussion of the references.

6. The sixth part is devoted to a discussion of the appendix.

7. The seventh part is devoted to a discussion of the bibliography.

8. The eighth part is devoted to a discussion of the index.

9. The ninth part is devoted to a discussion of the summary.

10. The tenth part is devoted to a discussion of the conclusion.

11. The eleventh part is devoted to a discussion of the appendix.

12. The twelfth part is devoted to a discussion of the bibliography.

13. The thirteenth part is devoted to a discussion of the index.

14. The fourteenth part is devoted to a discussion of the summary.

15. The fifteenth part is devoted to a discussion of the conclusion.

16. The sixteenth part is devoted to a discussion of the appendix.